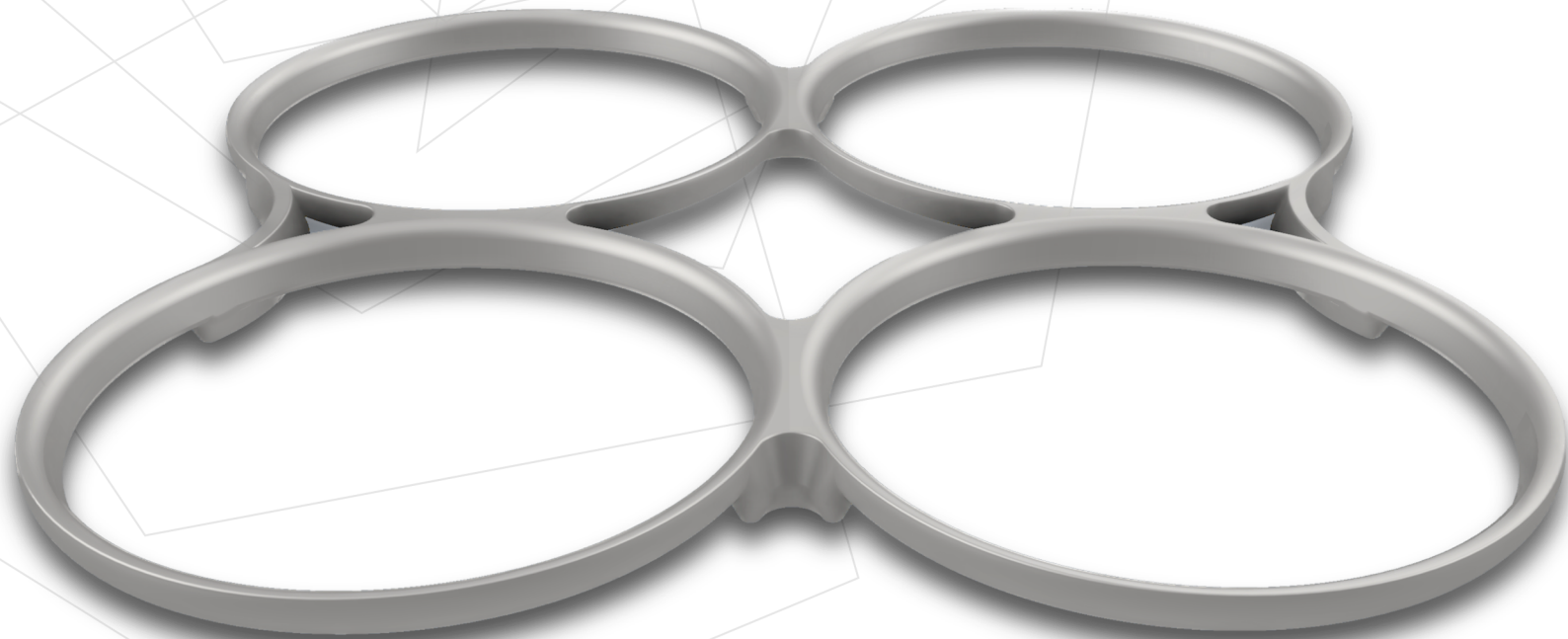




FINITE ELEMENT ANALYSIS OF A 3D PRINTED DRONE/QUADCOPTER BODY

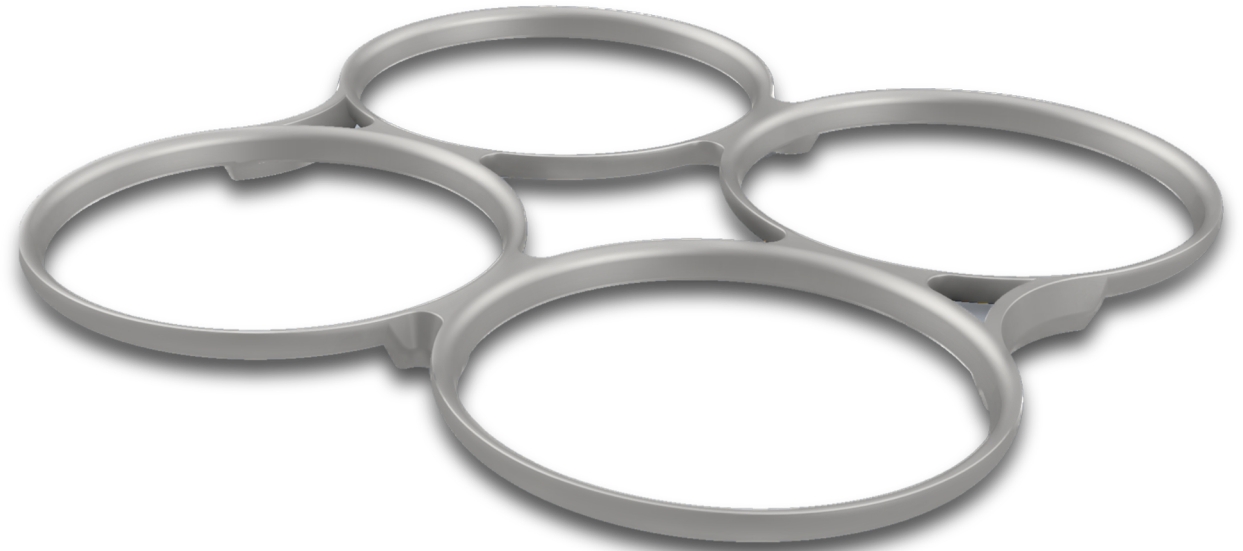
Abraham Martinez

Karl Johnson

Troy Schmidt

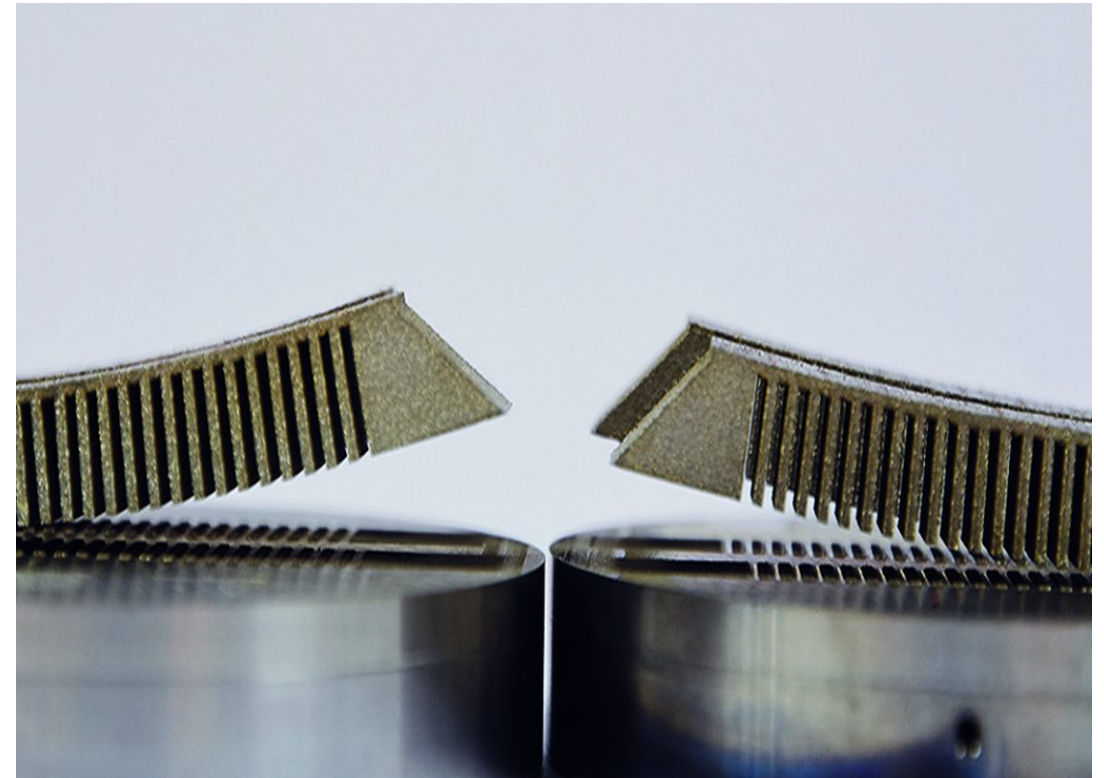
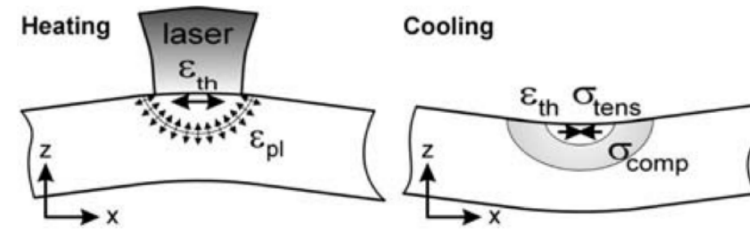
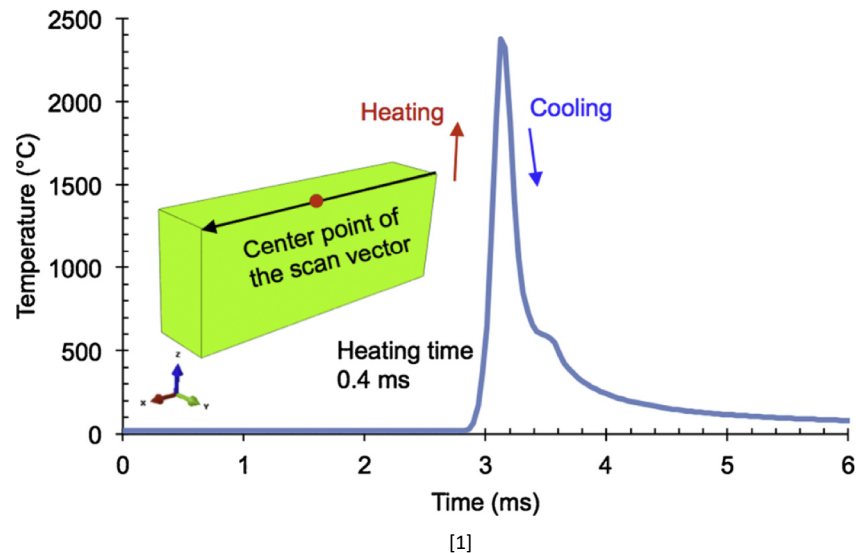
OBJECTIVE

- Model the additive manufacturing processes of a 3D printed drone body using ANSYS
- Analyze the effects of varying AM parameters on the outcome of the part.
 - Deformation
 - Residual Stresses
 - AM Solution Time
 - Temperature Study
- Optimize convergence & simulation time



INTRODUCTION- REASONS FOR AM SIMULATION

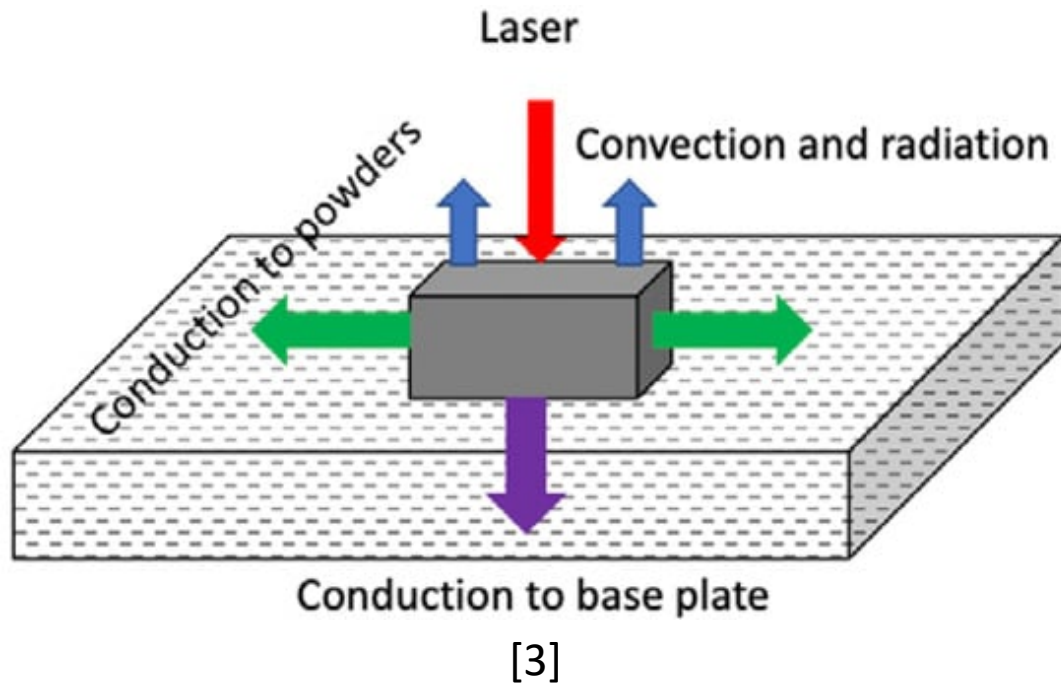
- Rapid heating and cooling leads to internal stresses
- Internal stress vastly reduces fatigue life
- Internal stress causes dimensional instability



INTRODUCTION- FUNDAMENTAL EQUATIONS

$$T = \frac{1}{4\pi KR(T - T_0)} \times \left\{ \underbrace{P \exp\left(\frac{-V(R+x)}{2D}\right)}_{\text{Heat input}} - A \left[\underbrace{h(T - T_0)}_{\text{Convection}} + \underbrace{\varepsilon\sigma(T^4 - T_0^4)}_{\text{Radiation}} + \underbrace{\frac{K(T - T_0)}{R}}_{\text{Conduction}} \right] \right\} + T_0$$

[3]



Coeff. Thermal expansion and elastic modulus Poisson's ratio Temperature Gradients

$$\sigma_{xx}(x, z) = -\frac{\alpha(T)E(T)}{1 - 2\nu(T)} \int_0^\infty \int_{-\infty}^\infty (G_{zh} \frac{\partial T}{\partial x}(x', z') + G_{xz} \frac{\partial T}{\partial z}(x', z')) dx' dz' + \frac{2z}{\pi} \int_{-\infty}^\infty \frac{p(s)(s-x)^2}{((s-x)^2 + z^2)^2} ds - \frac{\alpha(T)E(T)T(x, z)}{1 - 2\nu(T)}$$

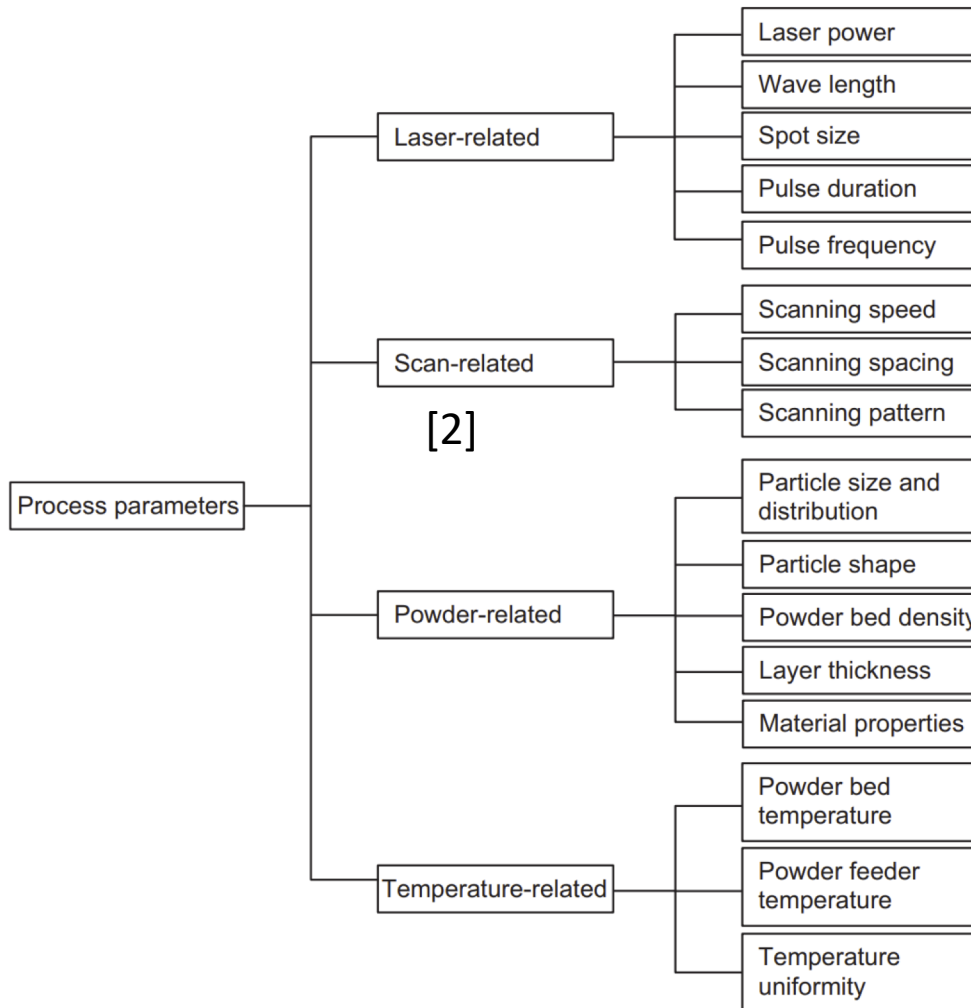
$$\sigma_{zz}(x, z) = -\frac{\alpha(T)E(T)}{1 - 2\nu(T)} \int_0^\infty \int_{-\infty}^\infty (G_{zh} \frac{\partial T}{\partial x}(x', z') + G_{zv} \frac{\partial T}{\partial z}(x', z')) dx' dz' + \frac{2z^3}{\pi} \int_{-\infty}^\infty \frac{p(s)}{((s-x)^2 + z^2)^2} ds - \frac{\alpha(T)E(T)T(x, z)}{1 - 2\nu(T)}$$

$$\sigma_{xz}(x, z) = -\frac{\alpha(T)E(T)}{1 - 2\nu(T)} \int_0^\infty \int_{-\infty}^\infty (G_{xzh} \frac{\partial T}{\partial x}(x', z') + G_{xzv} \frac{\partial T}{\partial z}(x', z')) dx' dz' + \frac{2z^2}{\pi} \int_{-\infty}^\infty \frac{p(s)(s-x)}{((s-x)^2 + z^2)^2} ds$$

$$\sigma_{yy}(x, z) = \nu(T)(\sigma_{xx} + \sigma_{zz}) - \alpha(T)E(T)T(x, z)$$

[3]

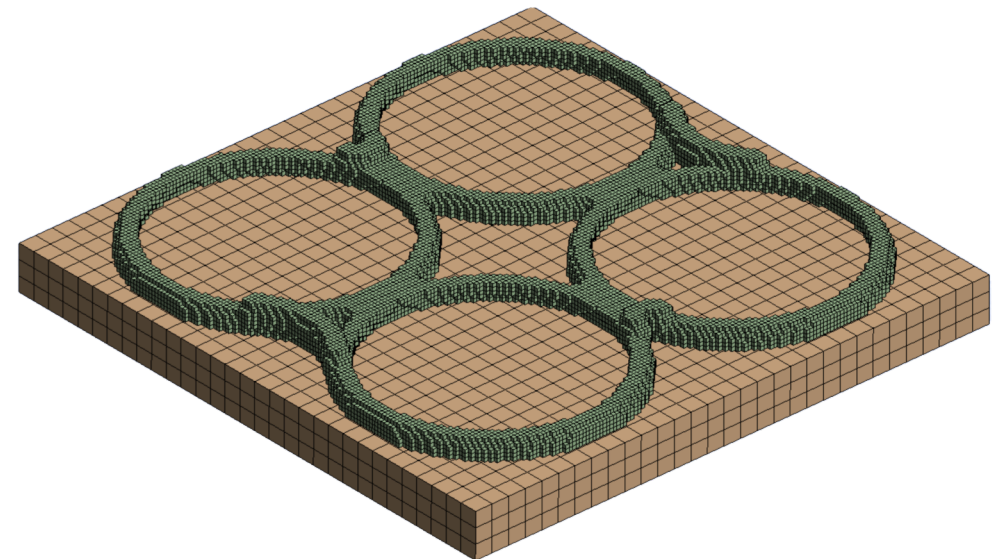
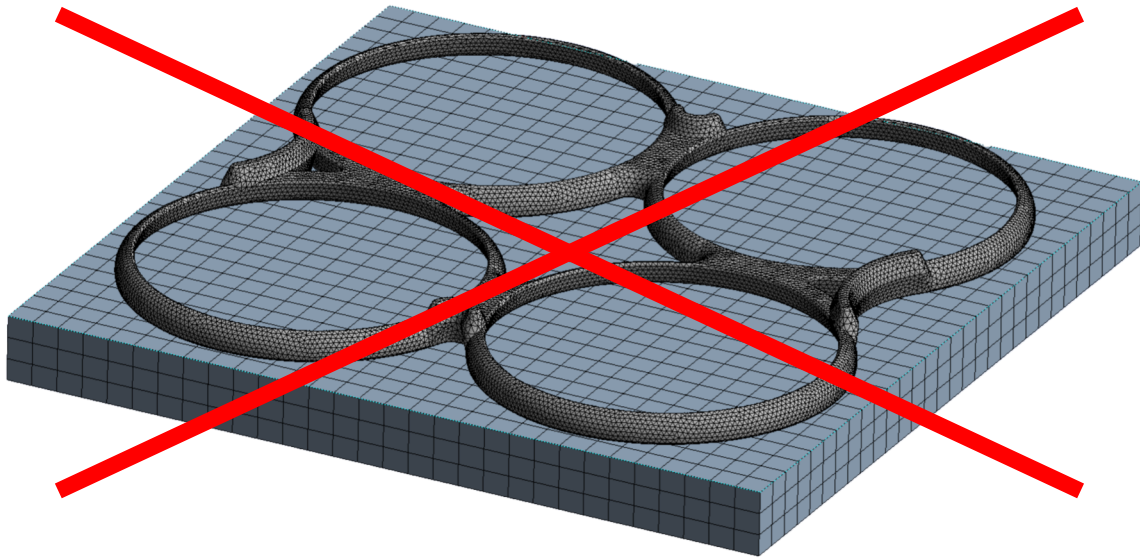
INTRODUCTION- AM PARAMETERS



- AM parameters shown have varying effects on the melt pool and residual stresses
- Scan speed: Increased speed decreases the linear energy density and lower temp gradient
- Laser power: Increased laser power increases temperature gradient
- Layer Thickness: increased thickness increases porosity and laser power
- Hatch spacing increased hatch spacing decreases build times but also increases porosity
- Not shown: Build Orientation

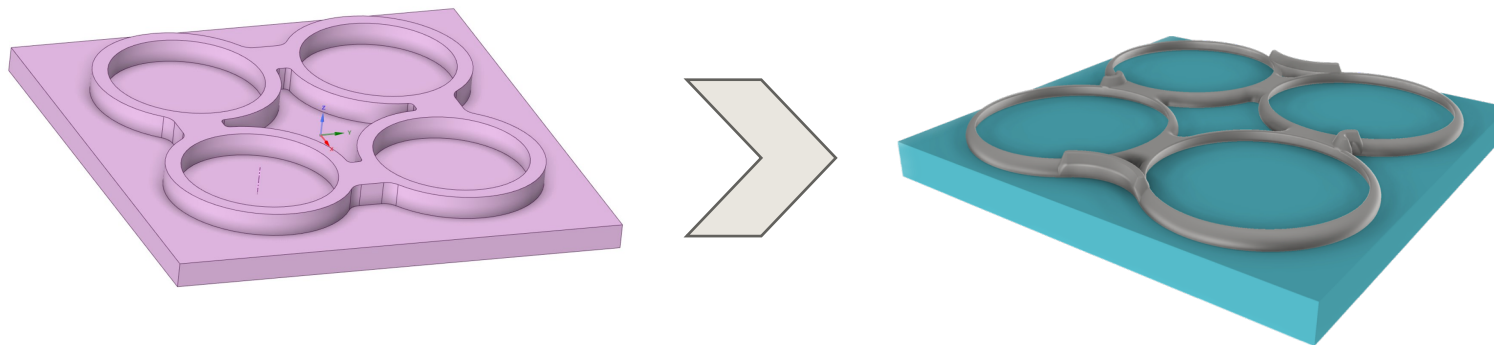
METHODOLOGY – MESH

- In additive manufacturing on ANSYS, the mesh must be layered
 - Geometries that vary with respect to their height typically require cartesian meshing to accommodate
 - Layered tetrahedron is also regularly used for ANSYS AM processes
 - Tetrahedron mesh will not solve



METHODOLOGY – AM PARAMETERS

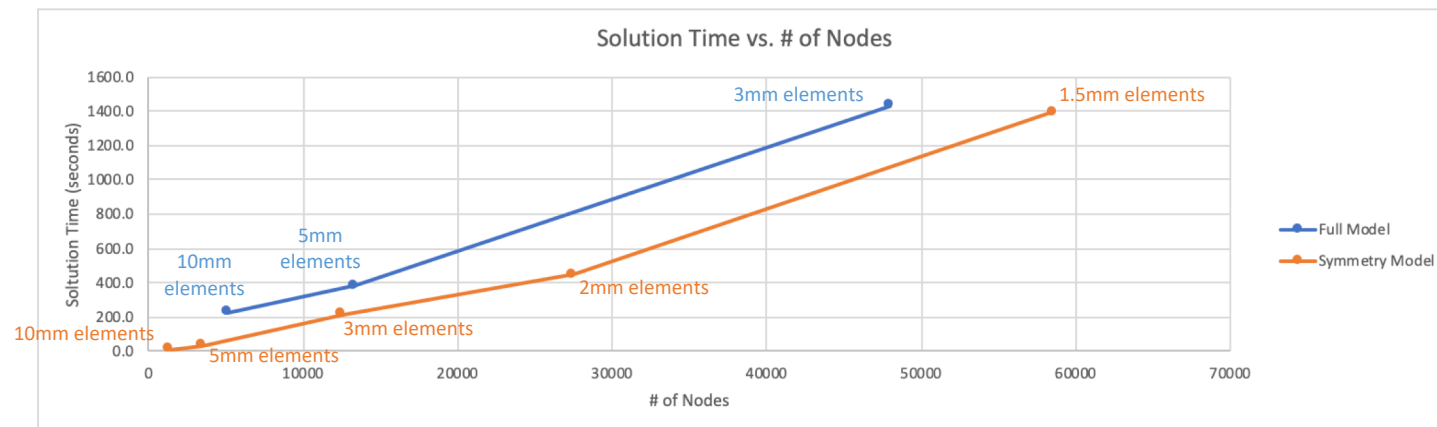
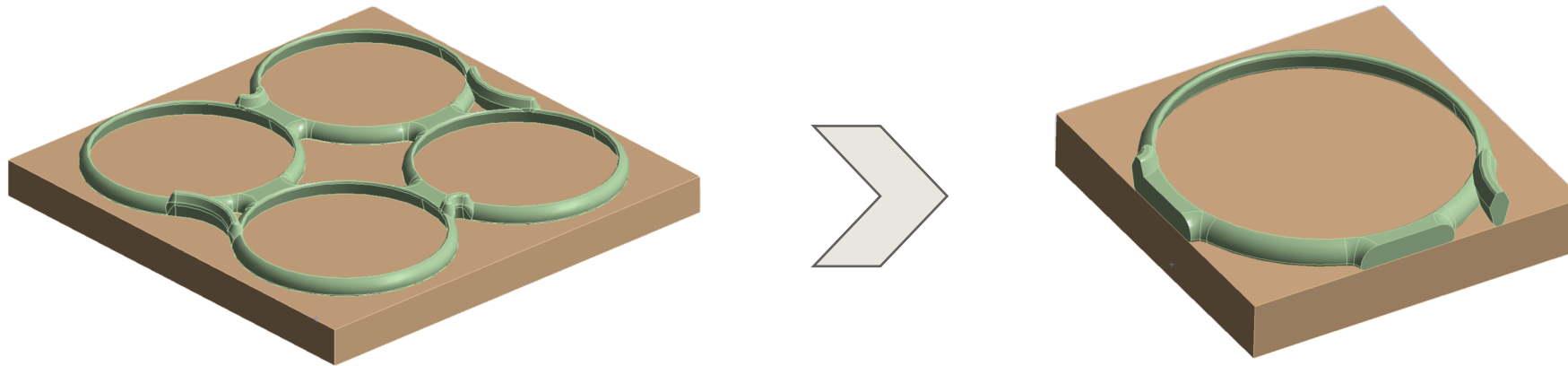
- 7.5mm mesh size for the first iteration
- 70C temperature at base plate
- Base plate, fixed support
- Baseplate and frame material, 316SS
- Part reference temperature 1370C
- Base reference temperature 50C
- Simplified geometry for first iteration, adding complexity to the model as issues were worked out.



Details of "Build Settings"	
Machine Settings	
Additive Process	Powder Bed Fusion
Inherent Strain	No
☐ Thermal Strain Scaling Factor	1.
☐ Deposition Thickness	5.e-002 mm
☐ Hatch Spacing	13. mm
☐ Scan Speed	1200. mm/s
Dwell Time	10. s
Dwell Time Multiple	1.
Number of Heat Sources	1
Build Conditions	
☐ Preheat Temperature	50. °C
Gas/Powder Temperature	Use Preheat Temperature
Gas Convection Coeff	1.e-005 W/mm ² .°C
Powder Convection Coeff	1.e-005 W/mm ² .°C
Powder Property Factor	1.e-002
Cooldown Conditions	
Room Temperature	22. °C
Gas/Powder Temperature	Use Room Temperature
Gas Convection Coeff	1.e-005 W/mm ² .°C
Powder Convection Coeff	1.e-005 W/mm ² .°C
Discretization Settings	
Layer Height	Program Controlled

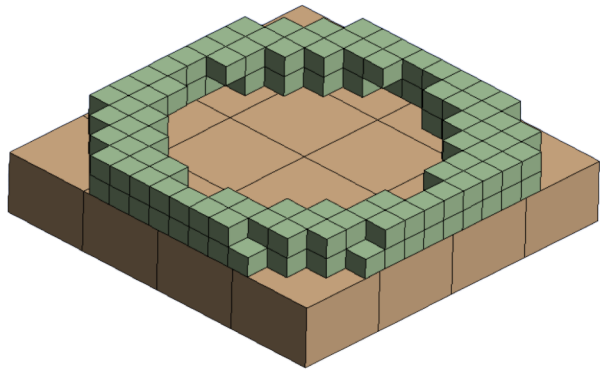
METHODOLOGY – SYMMETRY

- Apply double symmetry and add symmetry boundary conditions

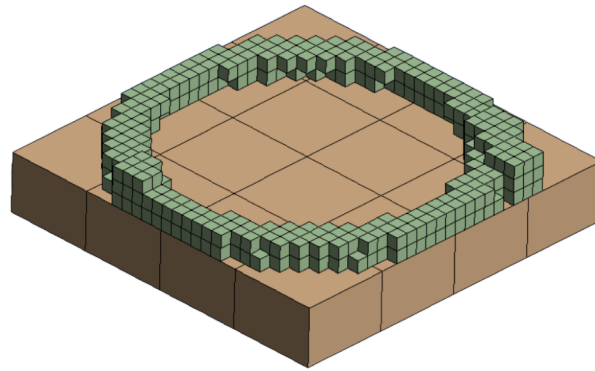


METHODOLOGY – CONVERGENCE

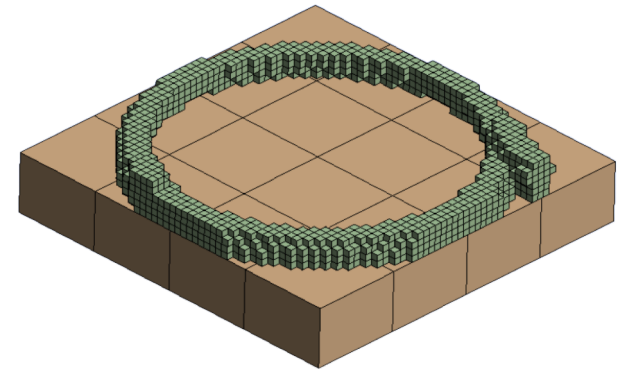
10mm elements



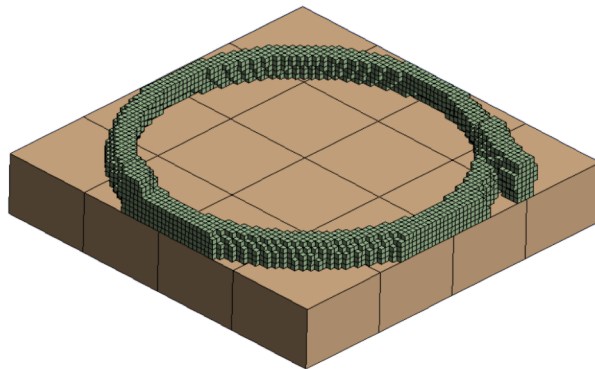
5mm elements



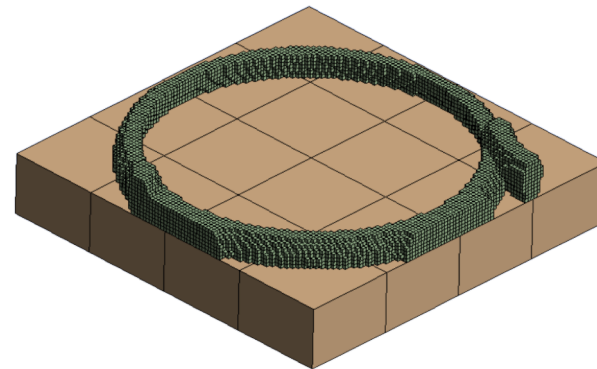
3mm elements



2mm elements

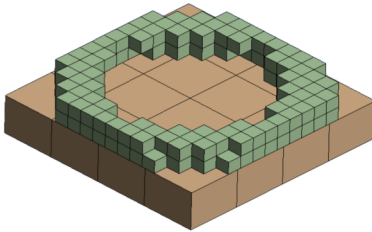


1.5mm elements

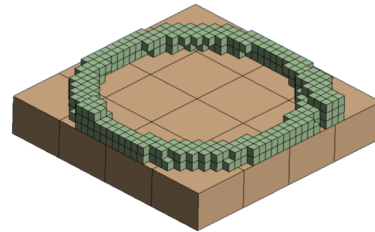


METHODOLOGY – CONVERGENCE

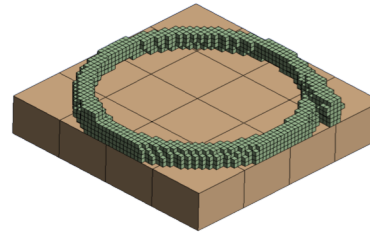
10mm elements



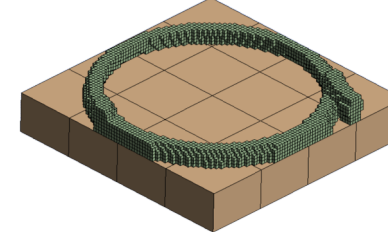
5mm elements



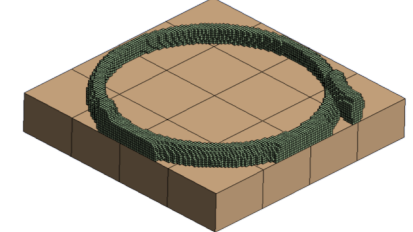
3mm elements



2mm elements



1.5mm elements



# of Elements	167
# of Nodes	1409
Max Deformation	1.082 mm
Max Von Mises Stress	417.39 MPa
Max Principle Stress	978.07 MPa
Thermal Solution Time	1.4 Seconds
Structural Solution Time	9.2 Seconds

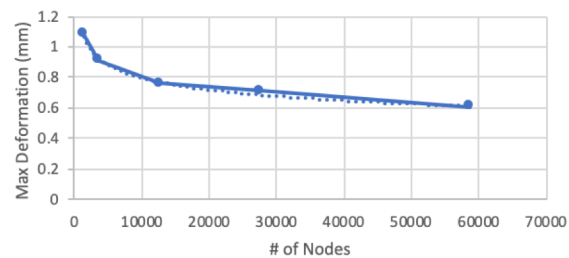
465
3515
0.91402 mm
487.18 MPa
1165.9 MPa
1.9 Seconds
34.3 Seconds

2041
12596
0.75691 mm
471.71 MPa
1148.9 MPa
9.5 Seconds
207.5 Seconds

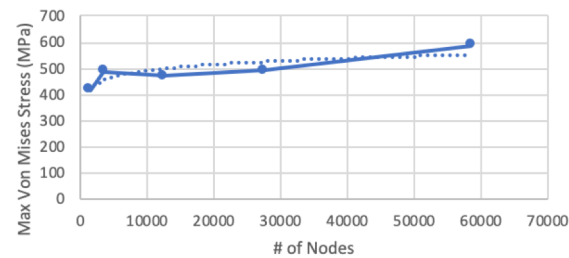
4844
27507
0.70786 mm
492.67 MPa
1200.6 MPa
23.0 Seconds
425.1 Seconds

11052
58579
0.60484 mm
586.41 MPa
2152.9 MPa
65.5 Seconds
1328.0 Seconds

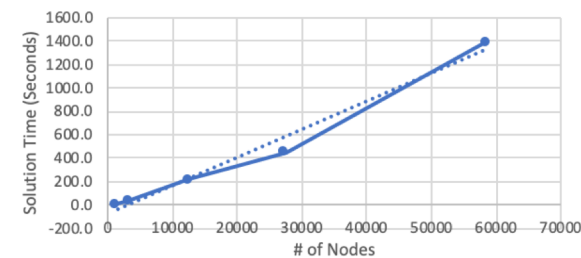
Max Deformation



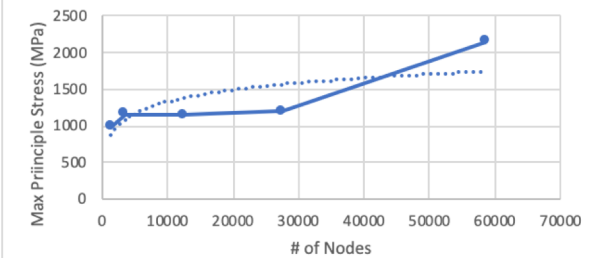
Max Von Mises Stress



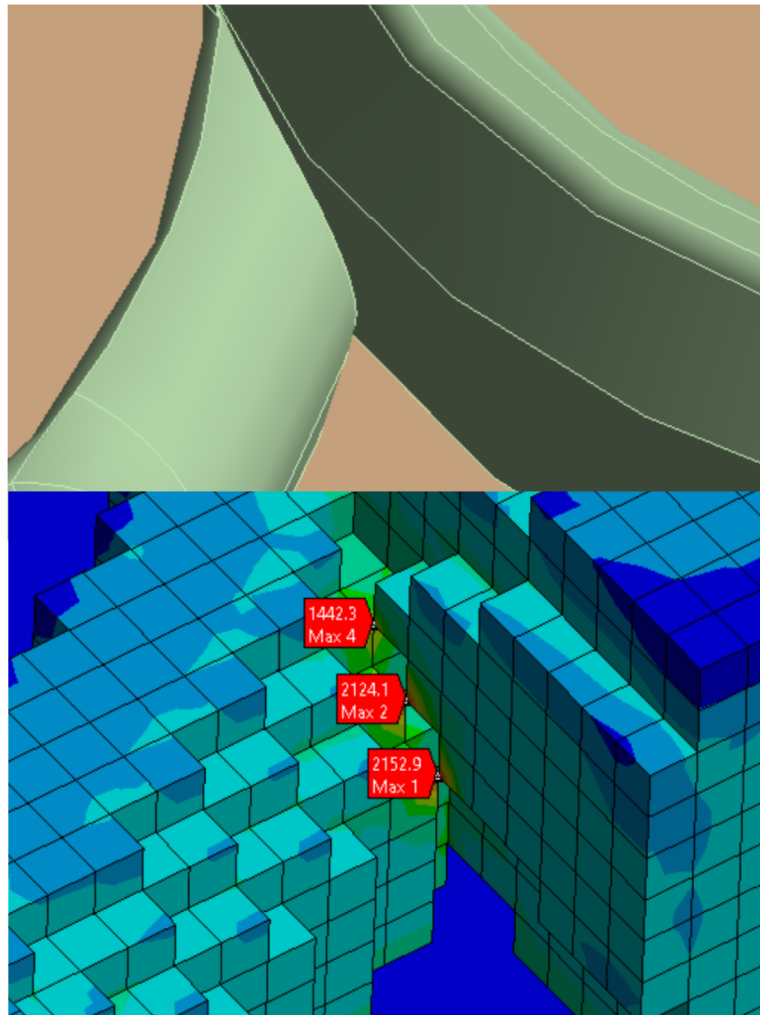
Solution Time vs. # of Nodes



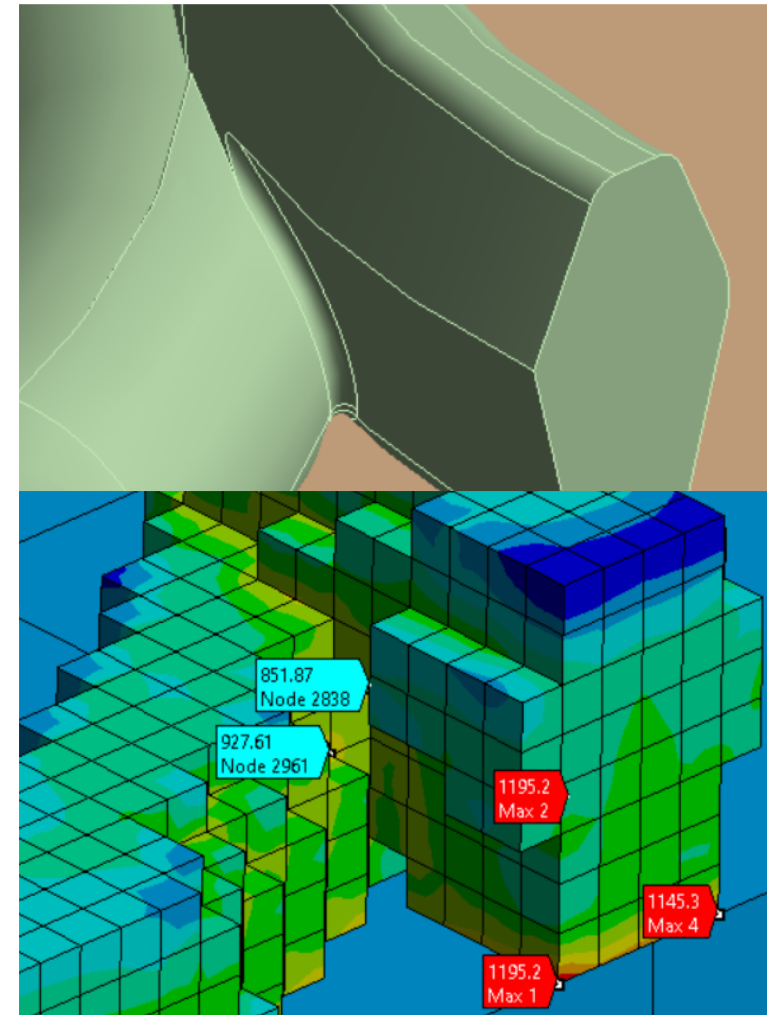
Max Principle Stress



METHODOLOGY – MODIFY GEOMETRY



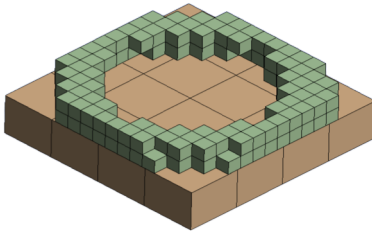
Max Principle Stress @ Sharp Corner: 2152.9 MPa



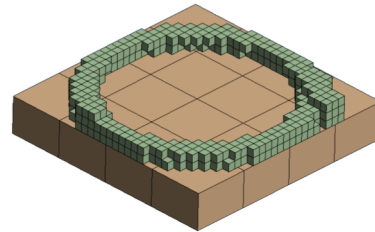
Max Principle Stress @ Fillet: 927.61 MPa

RESULTS – CONVERGENCE OF MODIFIED MODEL

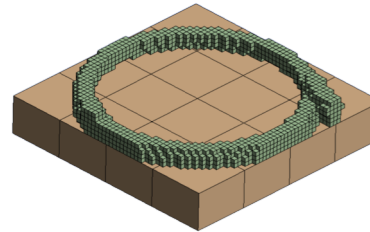
10mm elements



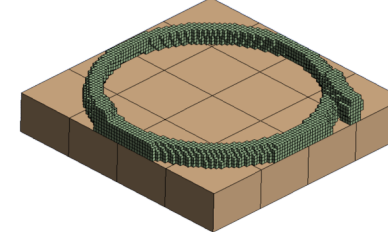
5mm elements



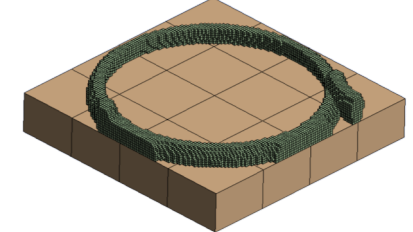
3mm elements



2mm elements



1.5mm elements
Modified Geometry



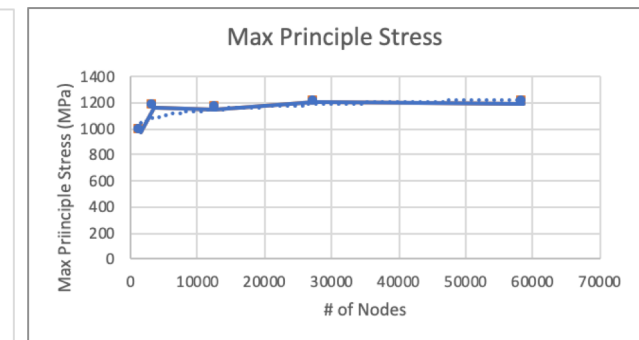
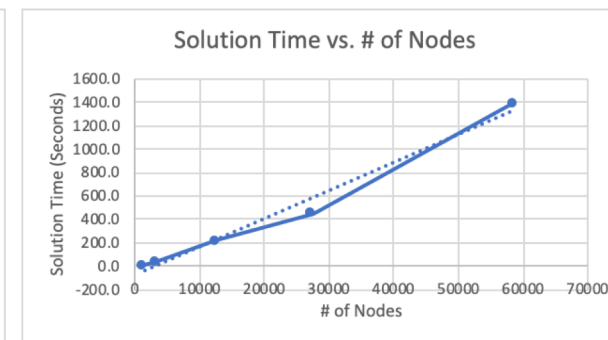
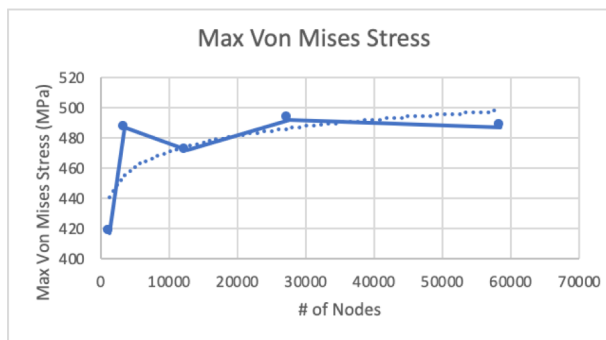
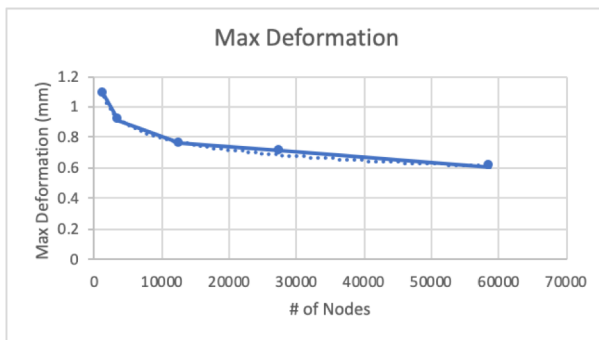
# of Elements	167
# of Nodes	1409
Max Deformation	1.082 mm
Max Von Mises Stress	417.39 MPa
Max Principle Stress	978.07 MPa
Thermal Solution Time	1.4 Seconds
Structural Solution Time	9.2 Seconds

# of Elements	465
# of Nodes	3515
Max Deformation	0.91402 mm
Max Von Mises Stress	487.18 MPa
Max Principle Stress	1165.9 MPa
Thermal Solution Time	1.9 Seconds
Structural Solution Time	34.3 Seconds

# of Elements	2041
# of Nodes	12596
Max Deformation	0.75691 mm
Max Von Mises Stress	471.71 MPa
Max Principle Stress	1148.9 MPa
Thermal Solution Time	9.5 Seconds
Structural Solution Time	207.5 Seconds

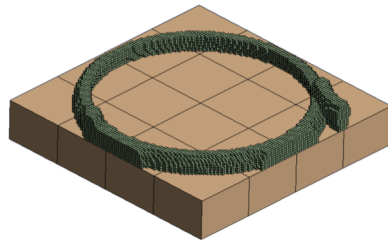
# of Elements	4844
# of Nodes	27507
Max Deformation	0.70786 mm
Max Von Mises Stress	492.67 MPa
Max Principle Stress	1200.6 MPa
Thermal Solution Time	23.0 Seconds
Structural Solution Time	425.1 Seconds

# of Elements	11052
# of Nodes	58579
Max Deformation	0.60484 mm
Max Von Mises Stress	487.3 MPa
Max Principle Stress	1195.2 MPa
Thermal Solution Time	65.2 Seconds
Structural Solution Time	1326.9 Seconds



RESULTS – TEMPERATURE STUDY

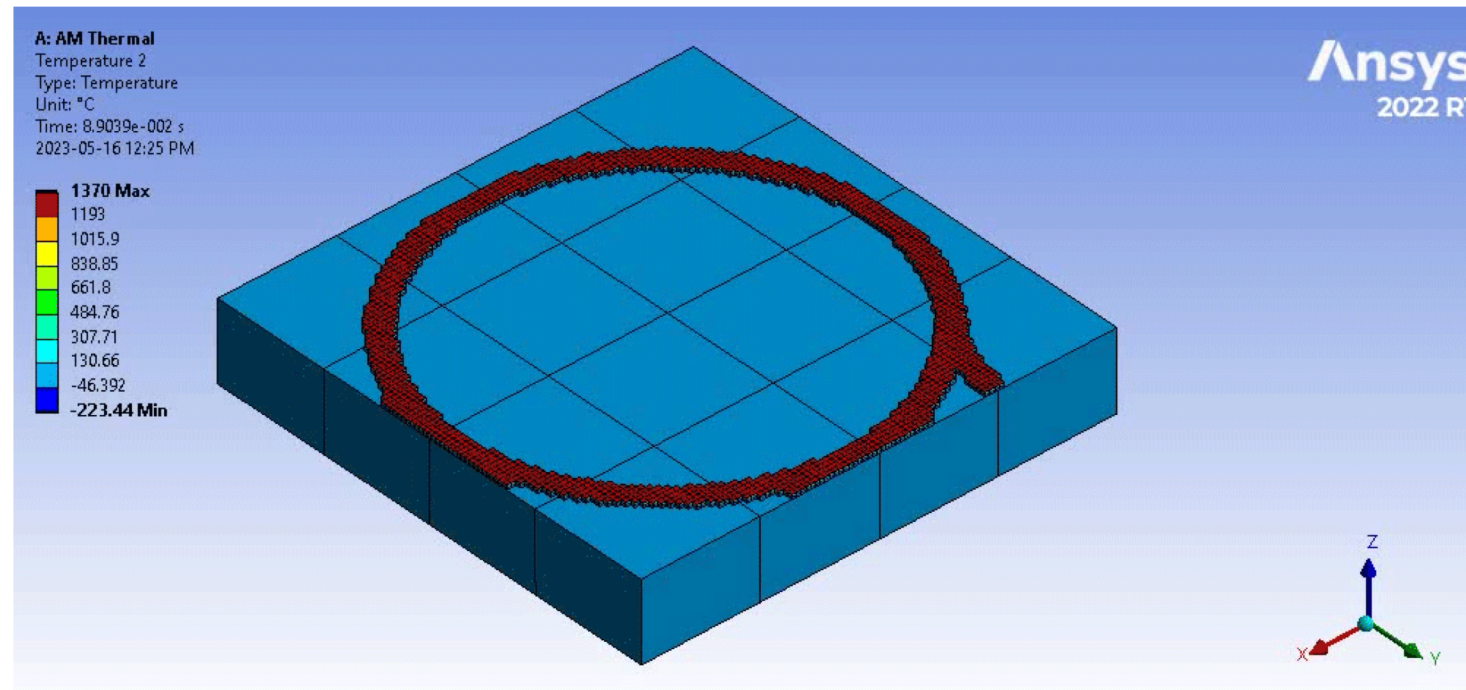
1.5mm elements



Build Time: 2632.2 S [44 minutes]

Cooldown Time: 3168.7 S [53 minutes]

TOTAL TIME: 1hr 37min



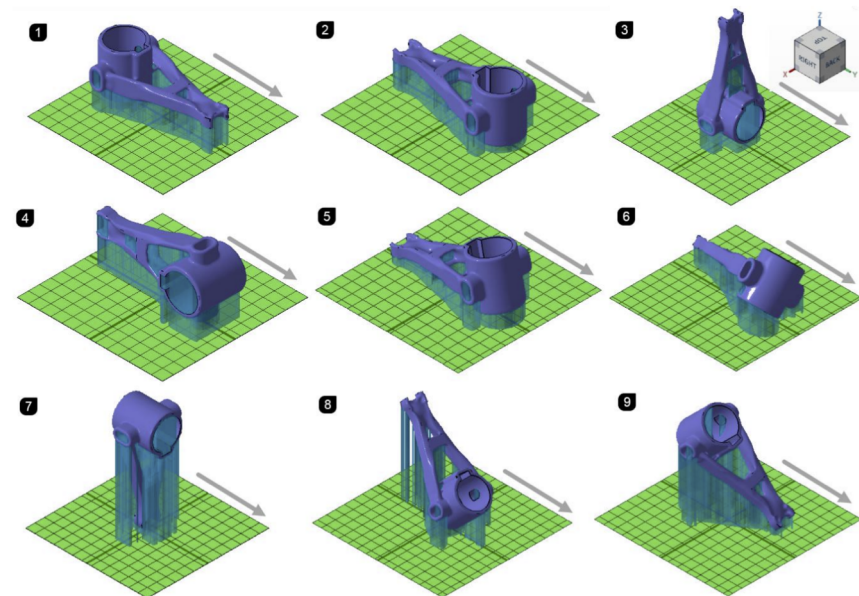
Transient Temperature during Build Step

DISCUSSION/ FUTURE CONSIDERATIONS

Material	Elastic Modulus	Conductivity	Coeff Thermal Expansion	Poissons ratio
Stainless steel	310 GPa	14.4 W/m•K	$16 \frac{10^{-6}m}{m \cdot C}$	.305
Titanium	120 GPa 	24.5 W/m•K 	$9 \frac{10^{-6}m}{m \cdot C}$ 	.32 
Aluminum	69 GPa 	247 W/m•K 	$24 \frac{10^{-6}m}{m \cdot C}$ 	.334 

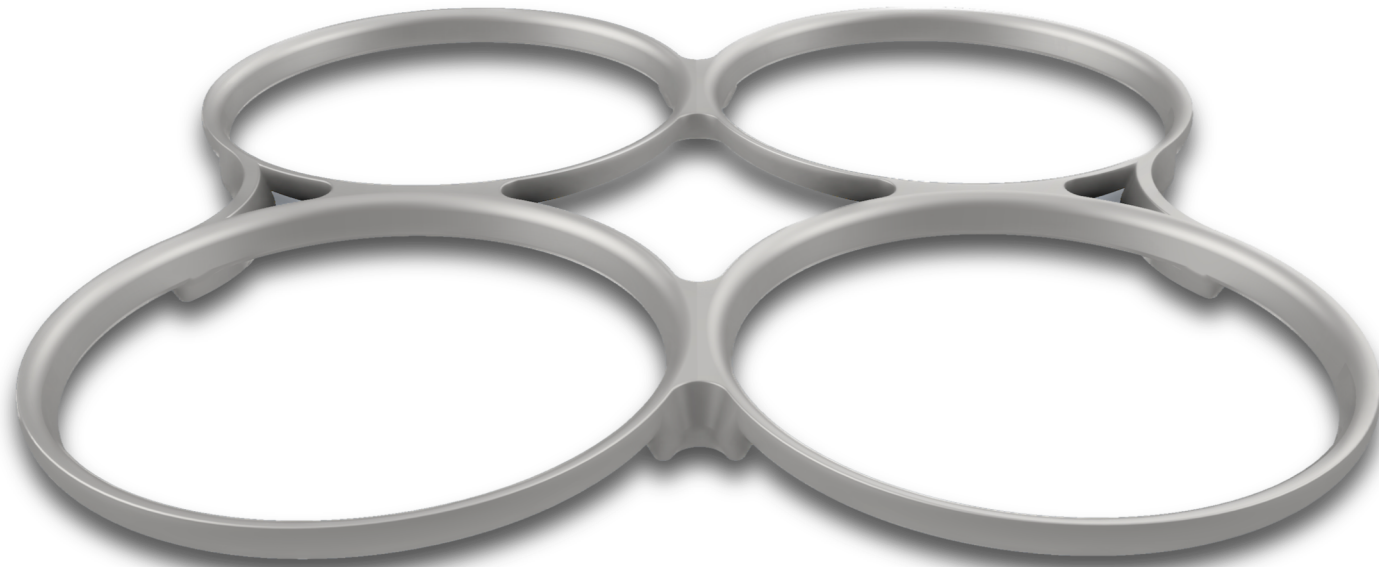
[7]

- Material
- Build orientation
- Part geometry
- Symmetry
- Node numbering
- Mesh type



[6]

CONCLUSION



A series of white, overlapping geometric lines and polygons on a black background, located on the left side of the slide.

THANK YOU

Abraham Martinez

Karl Johnson

Troy Schmidt

WORKS CITED

- [1] C. Li, J. F. Liu, X. Y. Fang, and Y. B. Guo, “Efficient predictive model of part distortion and residual stress in selective laser melting,” *Additive Manufacturing*, vol. 17, pp. 157–168, Oct. 2017, doi: <https://doi.org/10.1016/j.addma.2017.08.014>.
- [2] J.-P. Kruth, J. Deckers, E. Yasa, and R. Wauthlé, “Assessing and comparing influencing factors of residual stresses in selective laser melting using a novel analysis method,” *Proceedings of the Institution of Mechanical Engineers, Part B: Journal of Engineering Manufacture*, vol. 226, no. 6, pp. 980–991, Mar. 2012, doi: <https://doi.org/10.1177/0954405412437085>.
- [3] S. Sun, M. Brandt, and M. Easton, “Powder bed fusion processes,” *Laser Additive Manufacturing*, pp. 55–77, 2017, doi: <https://doi.org/10.1016/b978-0-08-100433-3.00002-6>.
- [4] E. Mirkoohi, H.-C. Tran, Y.-L. Lo, Y.-C. Chang, H.-Y. Lin, and S. Y. Liang, “Analytical Modeling of Residual Stress in Laser Powder Bed Fusion Considering Part’s Boundary Condition,” *Crystals*, vol. 10, no. 4, p. 337, Apr. 2020, doi: <https://doi.org/10.3390/cryst10040337>.
- [5] H. Hyer and C. M. Petrie, “Effect of powder layer thickness on the microstructural development of additively manufactured SS316,” vol. 76, pp. 666–674, Apr. 2022, doi: <https://doi.org/10.1016/j.jmapro.2022.02.047>.
- [6] R. Magana-Carranza, C. J. Sutcliffe, and E. A. Patterson, “The effect of processing parameters and material properties on residual forces induced in Laser Powder Bed Fusion (L-PBF),” 2021.
- [7] M. Pagac *et al.*, “Prediction of Model Distortion by FEM in 3D Printing via the Selective Laser Melting of Stainless Steel AISI 316L,” *Applied Sciences*, vol. 11, no. 4, p. 1656, Feb. 2021, doi: <https://doi.org/10.3390/app11041656>.
- [8] “Poisson’s ratio,” *Engineeringtoolbox.com*, 2019. https://www.engineeringtoolbox.com/poissons-ratio-d_1224.html
- [9] *Ansys® Workbench, Release 22.2*
- [10] Autodesk Inventor, 2022